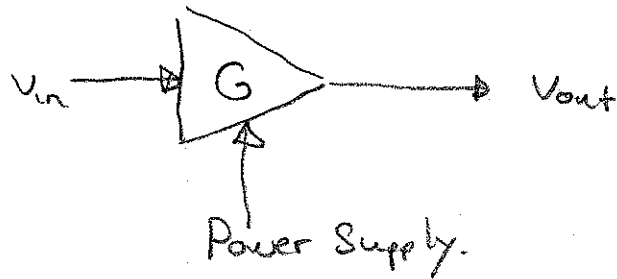
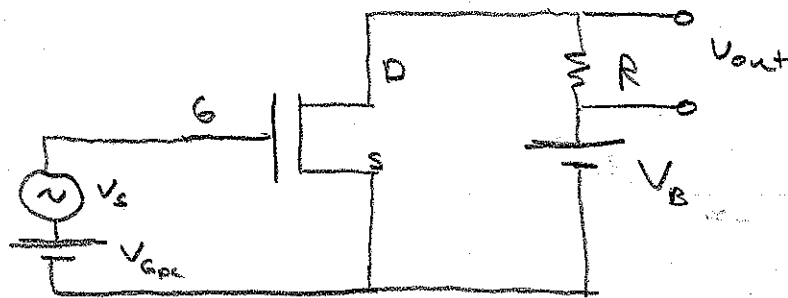


# Amplifier 1 dB compression Pt & 3rd Order Intercept.

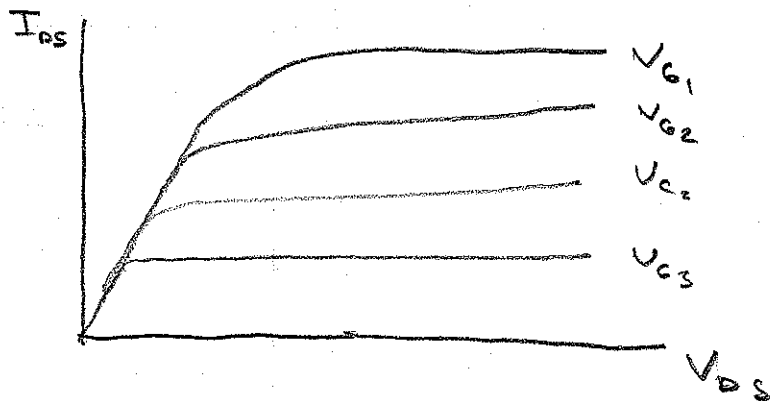


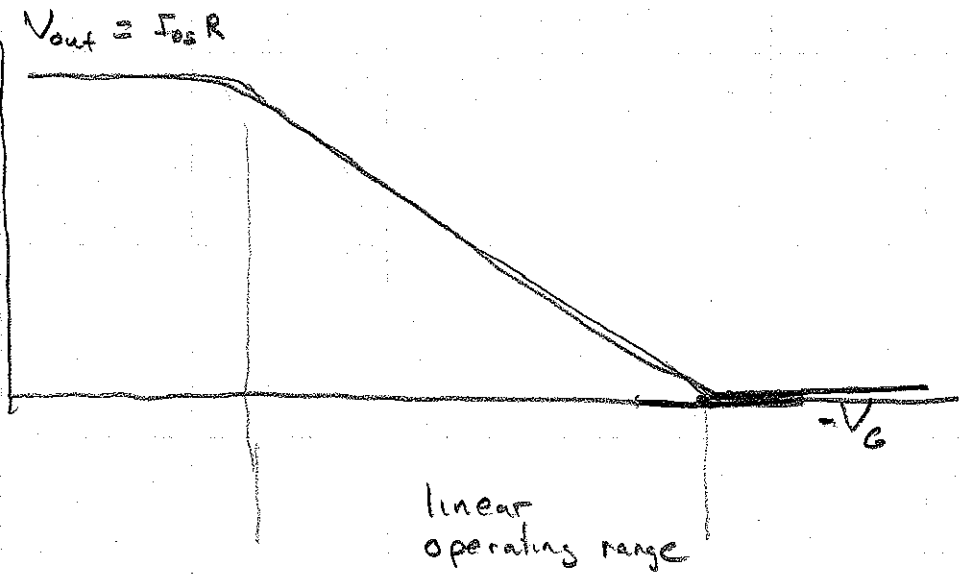
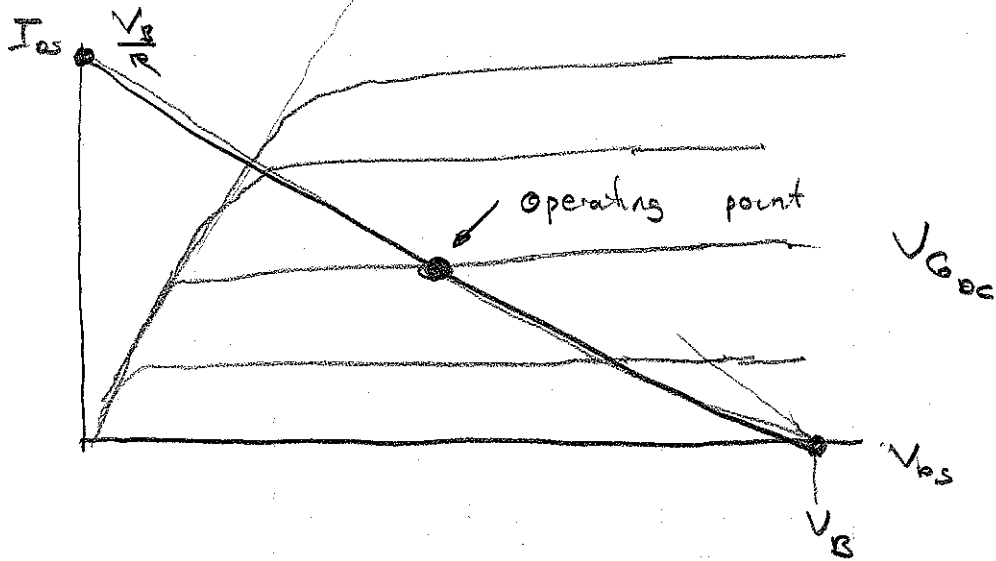
If there is a finite amount of power available from the power supply then there are limits to how large  $V_{out}$  can be.



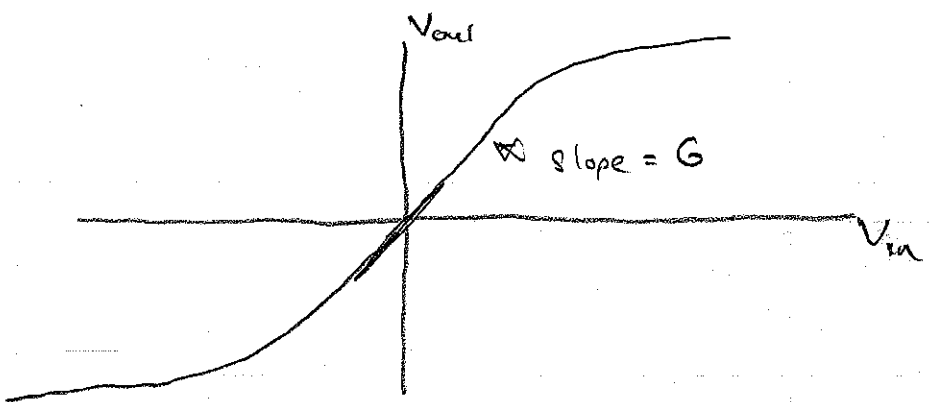
$$V_{DS} = V_B - I_{DS} R$$

FET V-I curve





Remove the bias for the time being.  
We can model a gain curve as



We can expand gain curve as a Taylor series

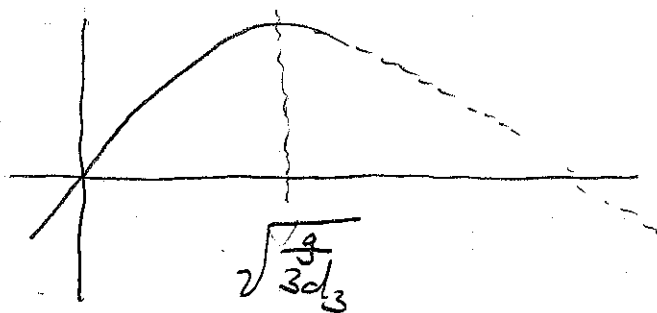
$$V_{out} = \cancel{V_B} + g V_{in} - \frac{d_2}{2} V_{in}^2 - \frac{d_3}{3} V_{in}^3 \dots$$

AC coupled
odd about  $V_{in}$

make sign gain roles over

For the time being, ignore  $d_2 > d_3$

$$V_{out} = g V_{in} - d_3 V_{in}^3$$



$$V_{inmax}^2 = \frac{g}{3d_3}$$

$$V_{max}^2 = \frac{g}{3d_3}$$

$$d_3 = \frac{g}{3V_{max}^2}$$

$$V_{out} = g \left( V_{in} - \frac{V_{in}^3}{3V_{max}^2} \right)$$

$$\text{Let } v_{in} = v_i \cos \omega t$$

$$\cos^3 x = \cos x \cos^2 x$$

$$= \cos x \left( \frac{1}{2} \cos 2x + \frac{1}{2} \right)$$

$$\cos^3 x = \frac{1}{2} \cos x \cos 2x + \frac{1}{2} \cos x$$

$$= \frac{1}{2} \left( \frac{1}{2} \cos x + \frac{1}{2} \cos 3x \right) + \frac{1}{2} \cos x$$

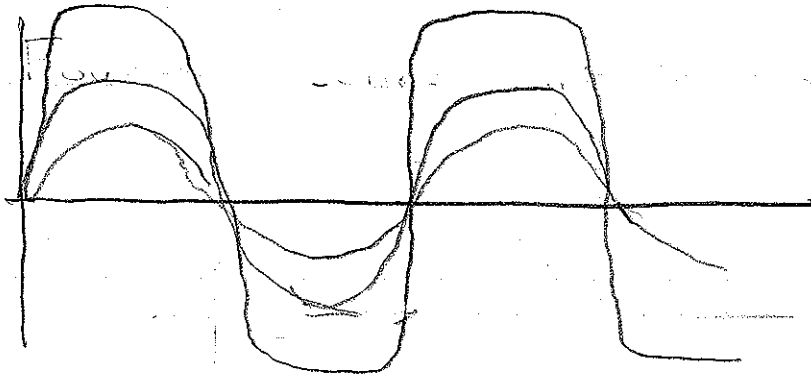
$$= \frac{3}{4} \cos x + \frac{1}{4} \cos 3x$$

$$v_{out} = g v_i \cos \omega t - \frac{g v_i^3}{3V_{max}^2} \left( \frac{3}{4} \cos \omega t + \frac{1}{4} \cos 3\omega t \right)$$

$$v_{out} = g \left( 1 - \left( \frac{v_i}{2V_{max}} \right)^2 \right) v_i \cos \omega t$$

$$- \frac{g}{3} \left( \left( \frac{v_i}{2V_{max}} \right)^2 \right) v_i \cos 3\omega t$$

Non-linearities generate harmonics!!



$$f(t) = \sum_{n=1}^{\infty} c_n \sin n \omega_0 t$$

$$c_n = \frac{4}{T} \int_0^{T/2} f(x) \sin n \frac{2\pi}{T} t dt$$

for square wave

$$c_n = \frac{4}{T} \int_0^{T/2} \sin \frac{2\pi n}{T} t dt$$

$$= -\frac{4}{T} \frac{T}{2\pi n} (\cos \pi n - 1)$$

$$= \frac{4}{\pi n} \text{ for } n \text{ odd}$$

$$= 0 \text{ for } n \text{ even.}$$

$$f(t) = \sum_{n=1}^{\infty} \frac{4}{\pi(2n-1)} \sin(2n-1)\omega_0 t$$

$\uparrow$  over  $n$                        $\uparrow$   $n$  odd

1 dB compression point.

Gain at the fundamental at low power

$$g_{\text{low}} = g$$

Gain at the fundamental at high power

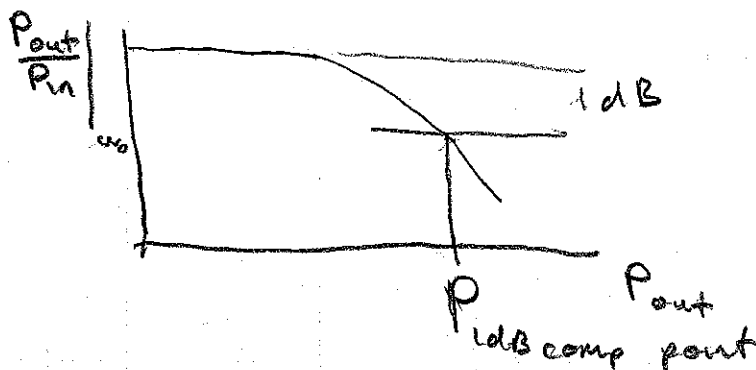
$$g_{\text{high}} = g \left( 1 - \left( \frac{V_i}{2V_{\text{max}}} \right)^2 \right)$$

$$\frac{g_{\text{high}}}{g_{\text{low}}} = \left( 1 - \left( \frac{V_i}{2V_{\text{max}}} \right)^2 \right)$$

$$10 \log \left( \left( \frac{g_{\text{high}}}{g_{\text{low}}} \right)^2 \right) = -1 \text{ dB}$$

is defined as the 1 dB compression point

Power at which the power gain at the fundamental at high power is 1 dB lower than the power gain at zero power



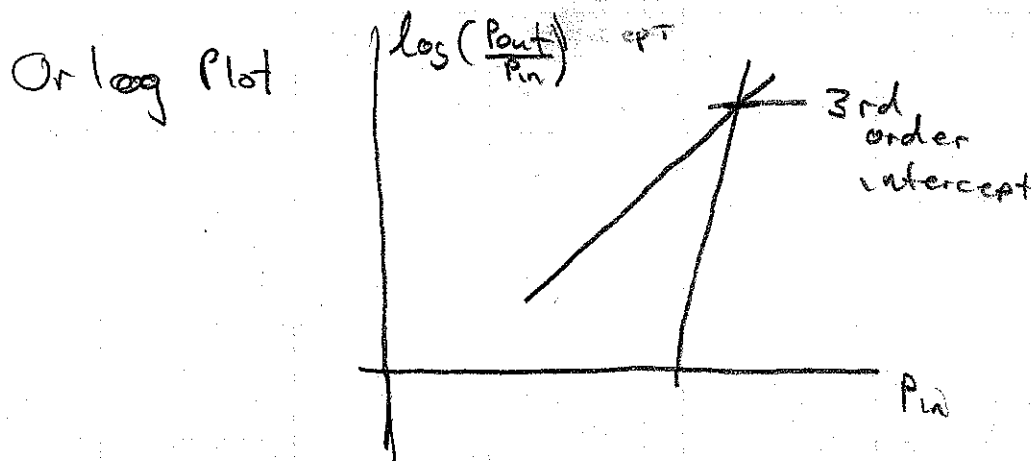
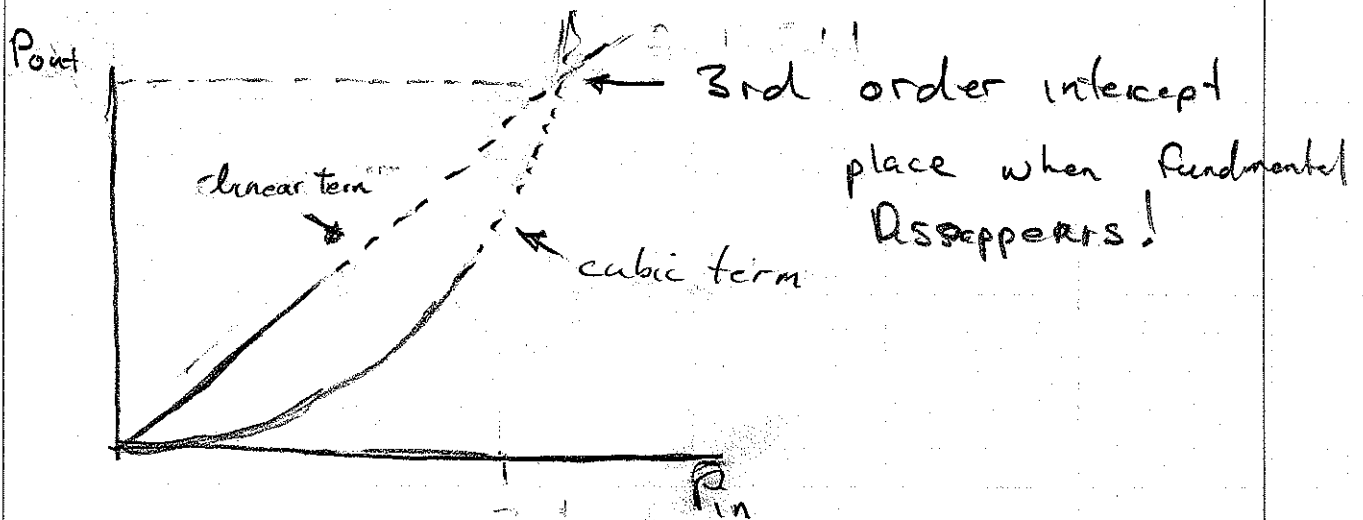
$$-1 \text{ dB} \Rightarrow 10^{-\frac{1}{10}} = (.794)$$

$$\left( \frac{V_{out}}{V_{in}} \left( \frac{V_i}{2V_{max}} \right)^2 \right)^2 = .794$$

$$\left( 1 - \left( \frac{V_i}{2V_{max}} \right)^2 \right) = .891$$

$$V_i = .66 V_{max} \text{ (for our simple model)}$$

3rd Order Intercept



Never really go to the 3rd order intercept  $\Rightarrow$  usually past the destroy level of the amplifier.

3rd order intercept

$$1 = \left( \frac{V_i}{2V_{max}} \right)^2 = 0$$

$$V_i = 2V_{max}$$

$$20 \log_{10} \left( \frac{V_i |_{\text{intercept}}}{V_i |_{-1\text{dBcomp}}} \right) = 9.63 \text{ dB}$$

$\therefore$  3rd order intercept  $\approx 10\text{dB}$  greater than the 1dB compression point.



3rd order Inter modulation Distortion.

$$v_{in} = v_1 \cos((\omega_0 + \Delta\omega)t) + v_2 \cos((\omega_0 - \Delta\omega)t)$$

$$v_{out} = g \left( v_{in} - \frac{v_{in}^3}{3V_{max}^2} \right)$$

$$(v_1 + v_2)^3 = v_1^3 + 3v_1^2 v_2 + 3v_1 v_2^2 + v_2^3$$

$$v_1^3 = \frac{3}{4} \cos((\omega_0 + \Delta\omega)t) + \frac{1}{4} \cos(3(\omega_0 + \Delta\omega)t)$$

$$v_2^3 = \frac{3}{4} \cos((\omega_0 - \Delta\omega)t) + \frac{1}{4} \cos(3(\omega_0 - \Delta\omega)t)$$

$$v_1^2 v_2 = \frac{1}{2} (1 + \cos 2(\omega_0 + \Delta\omega)t) \cos((\omega_0 - \Delta\omega)t)$$

$$= \frac{1}{2} \cos((\omega_0 - \Delta\omega)t)$$

$$+ \frac{1}{4} \cos((3\omega_0 + \Delta\omega)t) + \frac{1}{4} \cos(\omega_0 + 3\Delta\omega)t$$

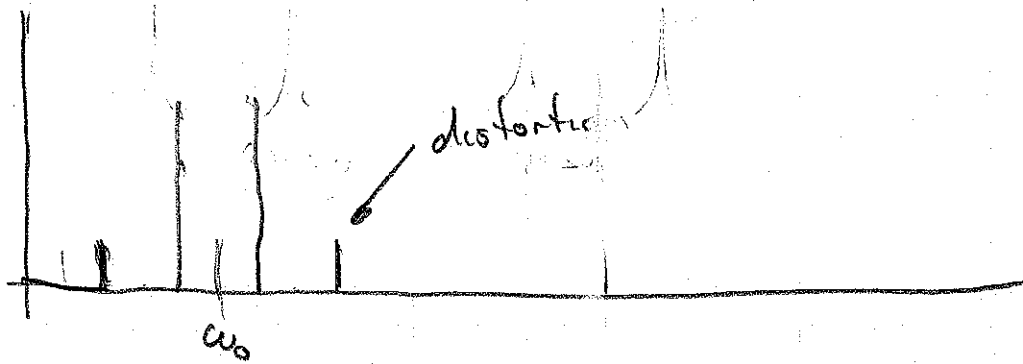
$$v_1 v_2^2 = \frac{1}{2} \cos((\omega_0 + \Delta\omega)t)$$

$$+ \frac{1}{4} \cos((3\omega_0 - \Delta\omega)t) + \frac{1}{4} \cos((\omega_0 - 3\Delta\omega)t)$$

Let

$$v_{in} = v_0 \cos((\omega + \Delta\omega)t) + v_0 \cos((\omega - \Delta\omega)t)$$

Assume  $\Delta\omega$  small



Amplitude of distortion products

$$= \frac{g}{3V_{max}^2} \frac{3}{4} (v_0)^3$$

$$= g v_0 \left( \frac{v_0}{2V_{max}} \right)^2$$

When  $v_0 = 2V_{max}$ , the amplitude of the distortion products match the linear power

⊙ To measure 3rd order intercept

- 1) Create two tones of same amplitude but different frequencies
- 2) Increase tone amplitude & measure distortion product compared to tone amplitude on a spectrum analyzer
- 3) Extrapolate when distortn products will match a linear signal

